



# ***High-Speed Photodetection Exploiting Quasi-Unipolar Charge Transport***

***P. D. Yoder***

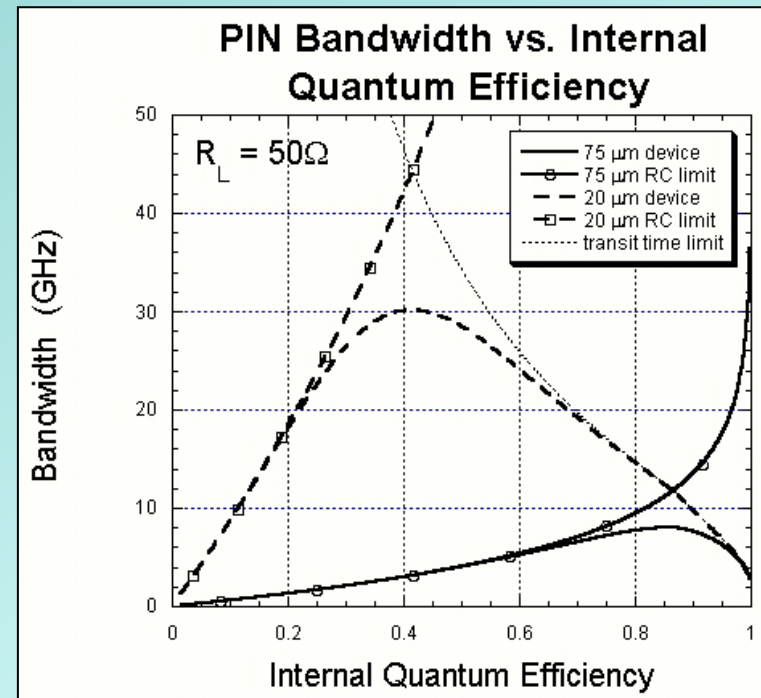
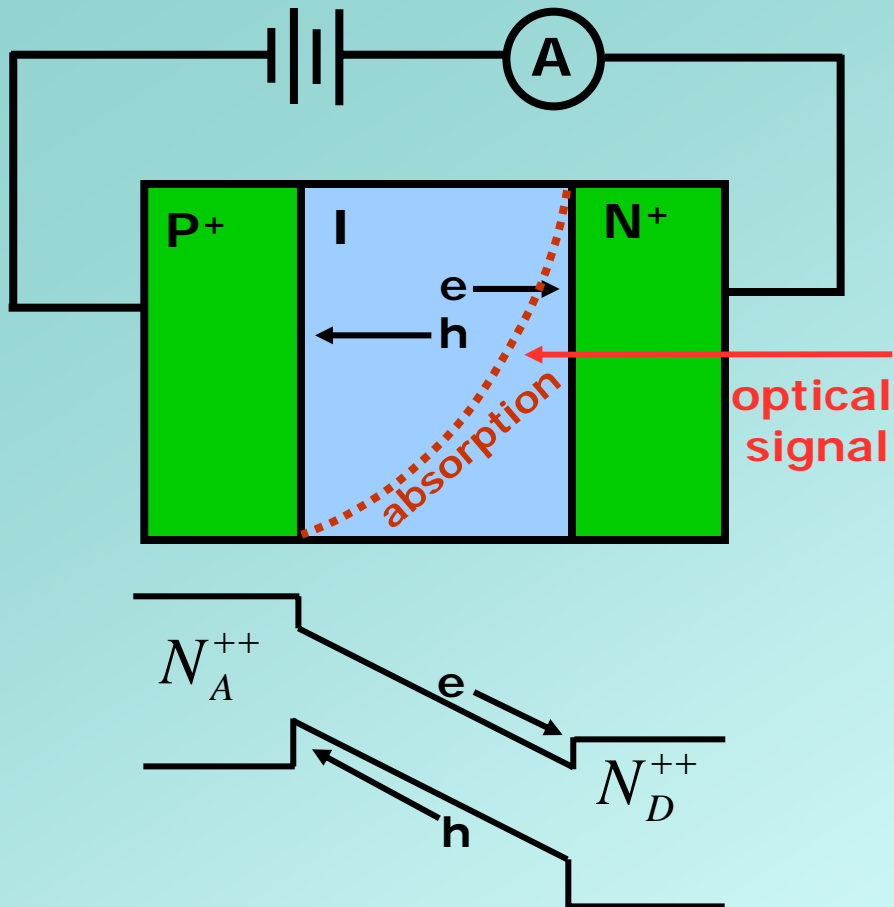
*School of Electrical and Computer Engineering  
Computational Electronics Group  
Georgia Institute of Technology*

# ***Outline***

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- *Background*
  - *Limitations of the heterojunction p-i-n design*
  - *Alternative design strategies*
- *Theory of the quasi-unipolar photodiode operation*
- *Device measurement*
- *Monte Carlo simulation*
- *Summary*

# The Heterojunction p-i-n Photodiode

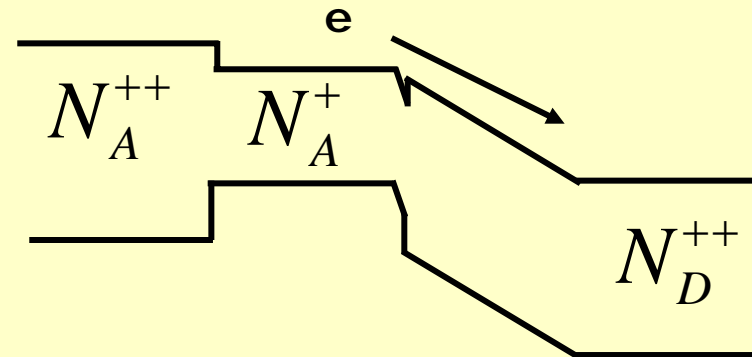


*High QE achieved at the cost of bandwidth*

# Alternative Design Strategies

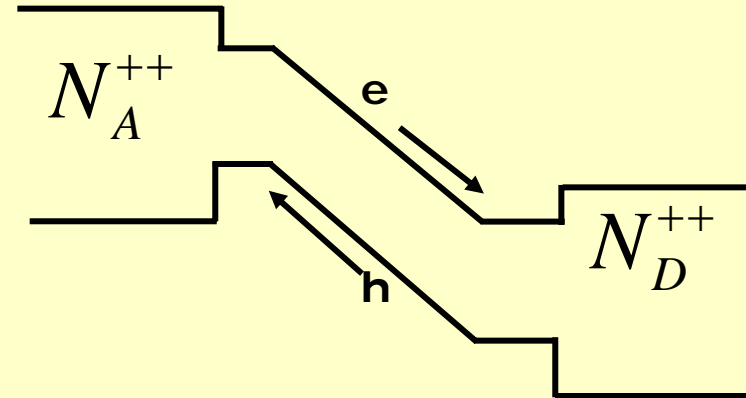
## • Uni-traveling Carrier (UTC)

• T. Ishibashi et al., *Jap. J. Appl. Phys.* **36**, 1997.



## • Partially Depleted Absorber (PDA)

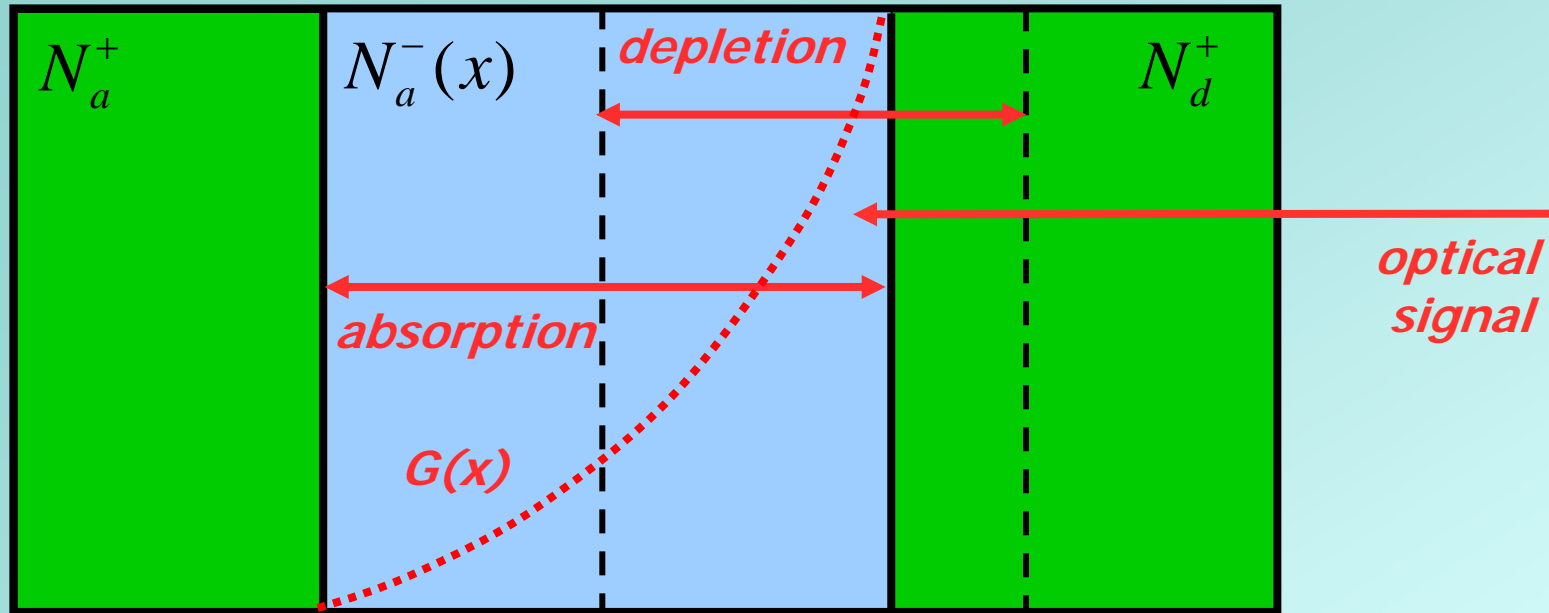
• D.A. Tulchinsky et al., *IEEE J. Selected Topics on Q. Mech.* **10**, 2004.



## • Quasi-Unipolar (QU)

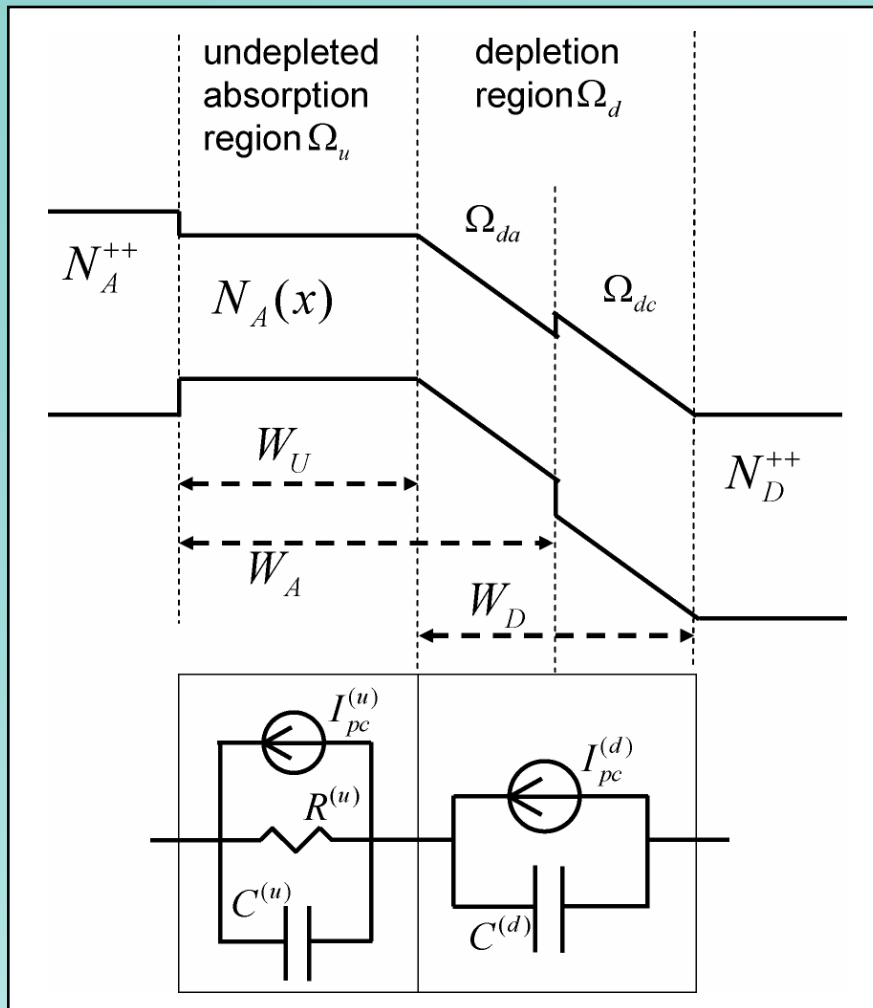
Yoder and Flynn, *J. Lightwave Tech.* **24**, 2006.

# *The Quasi-Unipolar Photodiode*



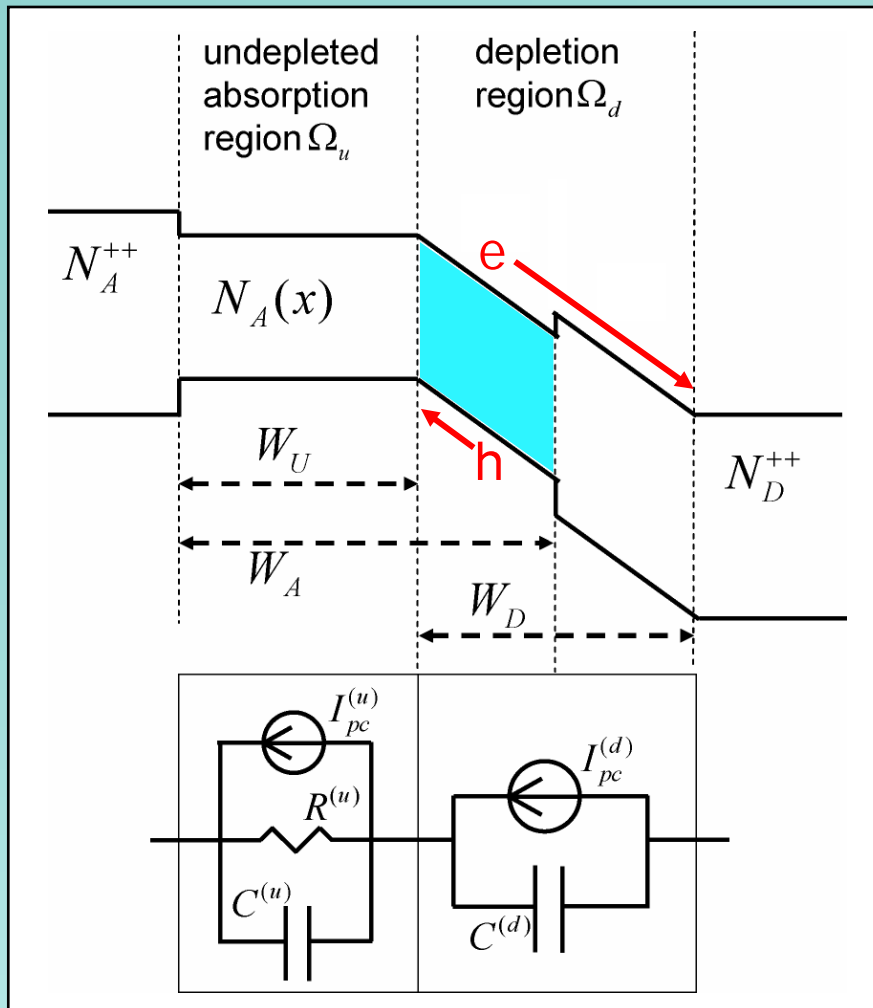
- Absorption and depletion regions are *overlapping*
- Depletion region offset is *controlled by doping and bias*
  - InP buffer doping
  - Zn diffusion profile through absorber

# QU Photodiode Design



- 3 independent design parameters
  - Absorber thickness ( $W_A$ )
  - Undepleted absorber width ( $W_U$ )
  - Depletion region thickness ( $W_D$ )
- Controlled by doping and bias

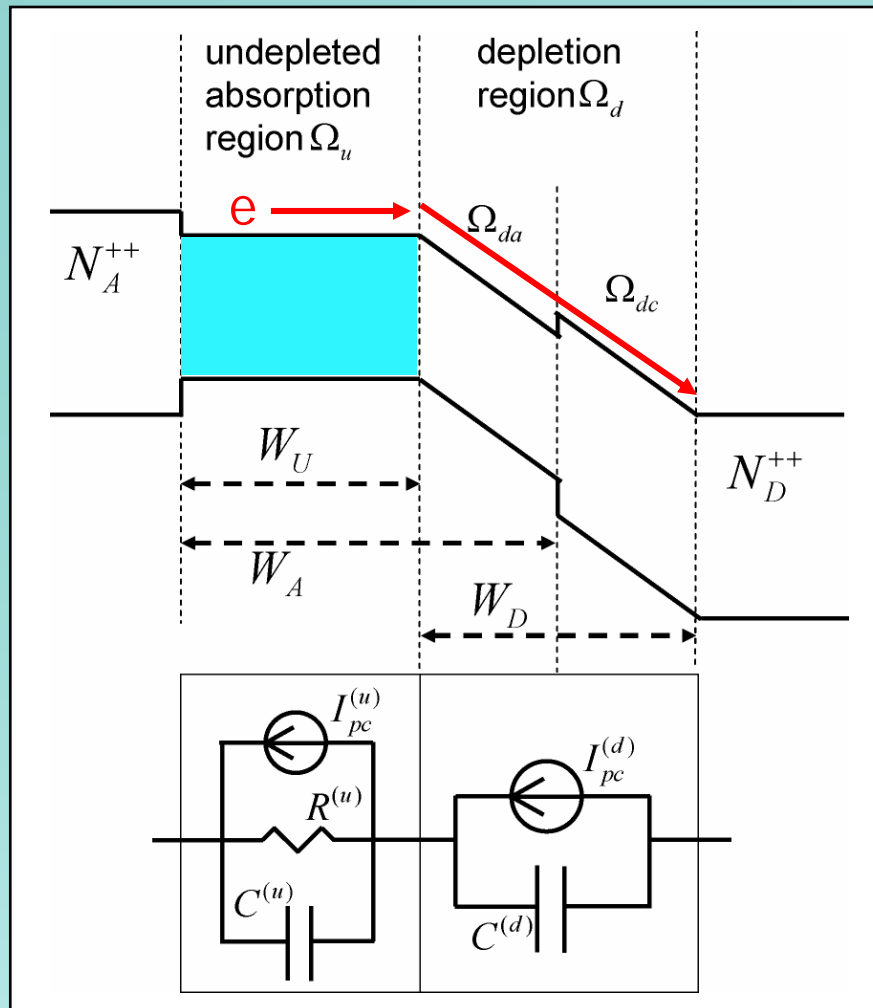
# Photogeneration in Depleted Absorber



- *E-h pairs generated within depleted absorber region drift to their respective depletion region edges*
- *Maximum hole transit distance limited to  $W_A - W_U$ .*

*Controlled by design!*

# Photogeneration in Undepleted Absorber



- *Electrons photogenerated within  $\Omega_u$  escape into  $\Omega_d$  by:*

- *Drift in static field*

$$E_{static} \approx \frac{k_B T}{q} \frac{\nabla N_A}{N_A}$$

- *Drift in dynamic field*

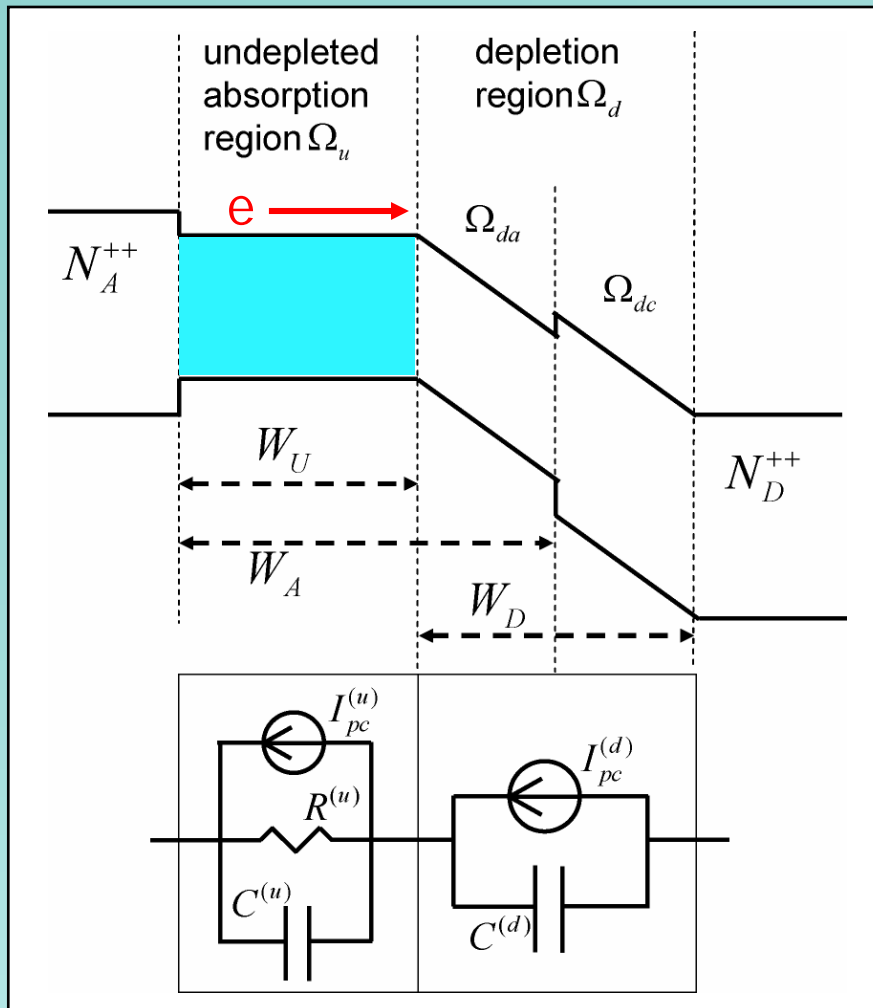
$$E_{dynamic} \approx J_{pc}^{(d)} / (q N_A \mu_p)$$

- *Diffusion*

$$\tau \approx W_U^2 / 2D_e$$

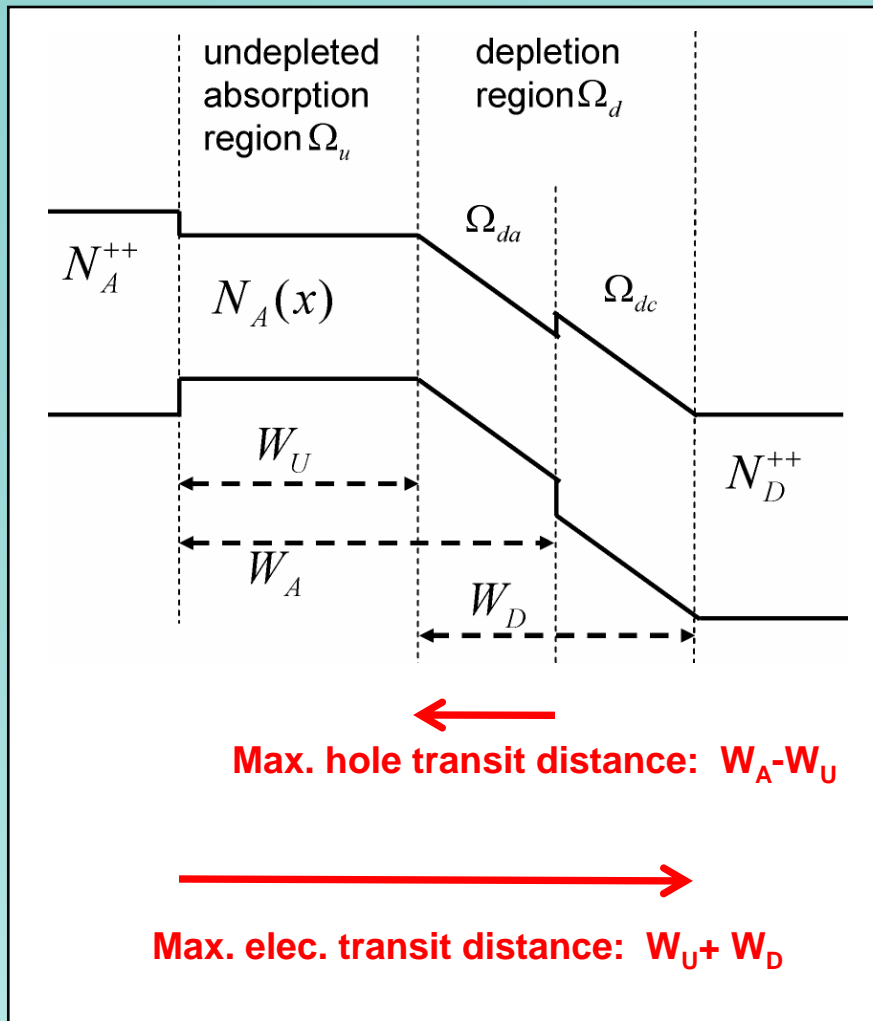


# QU Photodiode Operation



- *Electron motion in  $\Omega_u$  is decoupled from external circuit*
- *Holes generated within  $\Omega_u$  do not contribute to photocurrent*
- *Fraction of photocurrent carried by holes depends on  $W_u$  and  $W_D$*
- *Maximum electron transit distance limited to  $W_u + W_D$*   
***Controlled by design!***
- *Electron transit distance always shorter than for UTC device*

# QU Photodiode Operation



For arbitrary  $W_A$  and  $W_D$ :

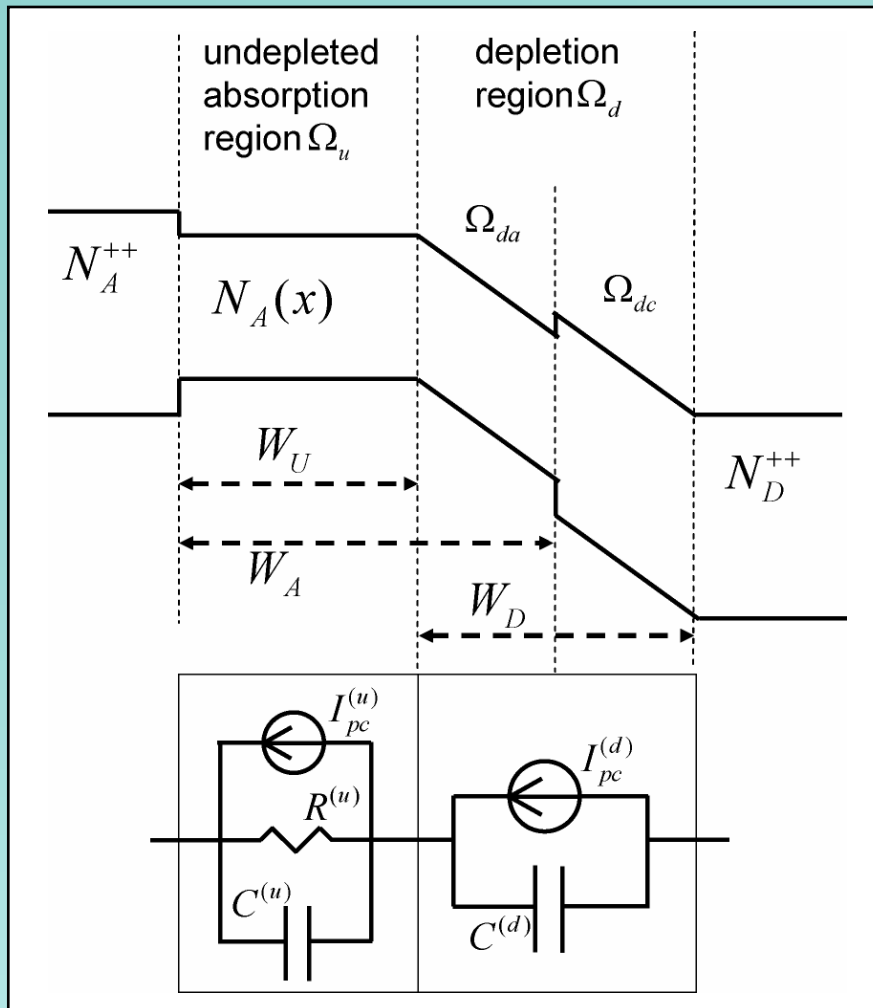
*Increasing  $W_U$  from 0 to  $W_A$*

- *Reduces the number of holes participating in photocurrent*

- *Trades electron against hole transit time*

*3dB bandwidth is approximately maximized when temporal extent of electron and hole photocurrent response to an optical impulse are "balanced".*

# QU Photodiode Operation



Limiting cases of QU design:

- UTC device:  $W_U \rightarrow W_A$
- *p-i-n*:  $W_U \rightarrow 0$ ,  $W_D \rightarrow W_A$
- PDA:  $W_U + W_D < W_A$

# Analytic Model: Linearized Moments of BTE

Within  $\Omega_u$  (undepleted absorber material):

$$\left( \frac{\partial}{\partial t} \left( 1 + \tau_p^{(u)} \frac{\partial}{\partial t} \right) + \frac{e\mu_p p_0}{\varepsilon} \right) \delta p - D_p \nabla^2 \delta p + \mu_p \vec{E}_0 \cdot \nabla \delta p = \frac{e\mu_p p_0}{\varepsilon} \delta n + \left( 1 + \tau_p^{(u)} \frac{\partial}{\partial t} \right) G(x, t)$$
$$\frac{\partial}{\partial t} \left( 1 + \tau_n \frac{\partial}{\partial t} \right) \delta n - D_n \nabla^2 \delta n + v_n \nabla \delta n = \left( 1 + \tau_n \frac{\partial}{\partial t} \right) G(x, t)$$

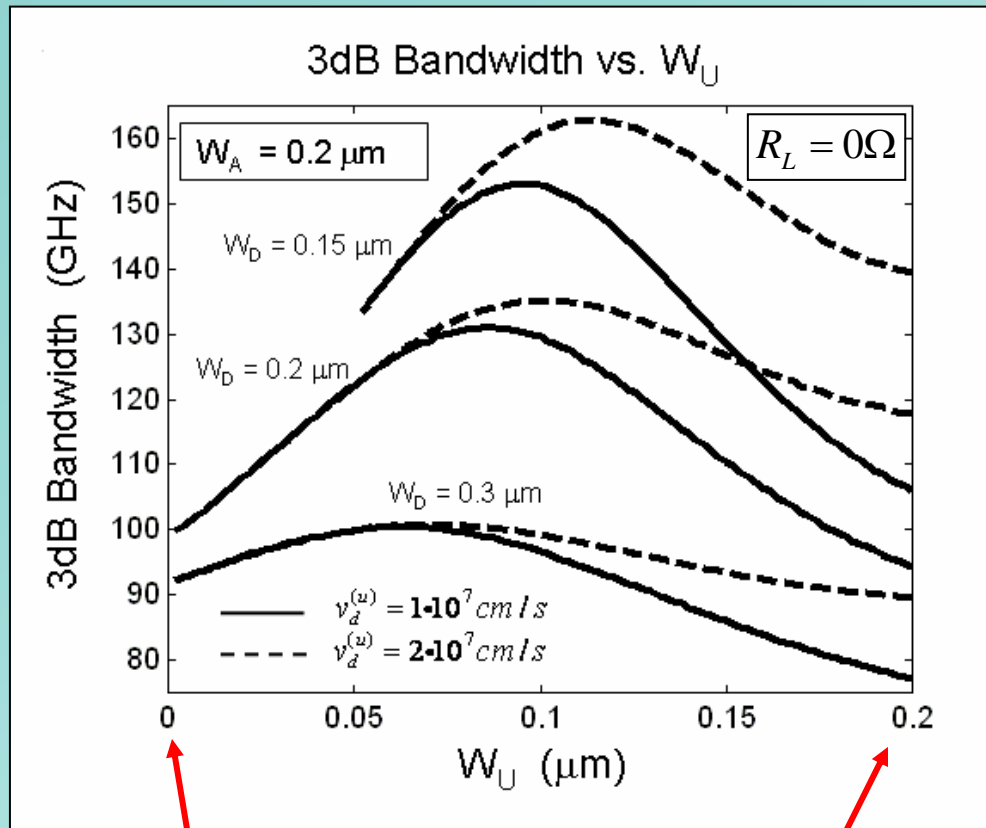
Within  $\Omega_{du}$  (depleted absorber material):

$$\frac{\partial}{\partial t} \left( 1 + \tau_p \frac{\partial}{\partial t} \right) \delta p - D_p \nabla^2 \delta p + v_p \nabla \delta p = \left( 1 + \tau_p \frac{\partial}{\partial t} \right) G(x, t)$$
$$\frac{\partial}{\partial t} \left( 1 + \tau_n \frac{\partial}{\partial t} \right) \delta n - D_n \nabla^2 \delta n + v_n \nabla \delta n = \left( 1 + \tau_n \frac{\partial}{\partial t} \right) G(x, t)$$

Within  $\Omega_{dc}$  (depleted collector material):

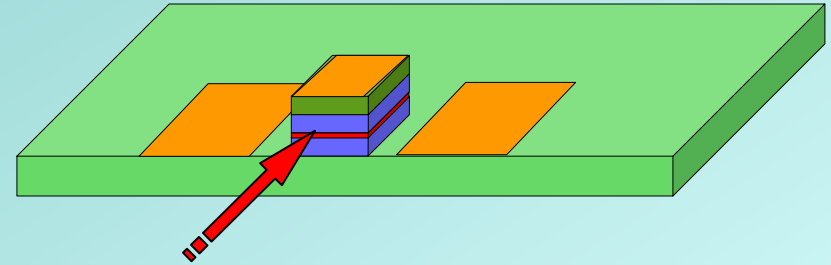
$$\frac{\partial}{\partial t} \left( 1 + \tau_n \frac{\partial}{\partial t} \right) \delta n - D_n \nabla^2 \delta n + v_n \nabla \delta n = \left( 1 + \tau_n \frac{\partial}{\partial t} \right) G(x, t)$$

# Application to QU Waveguide Geometry Designs



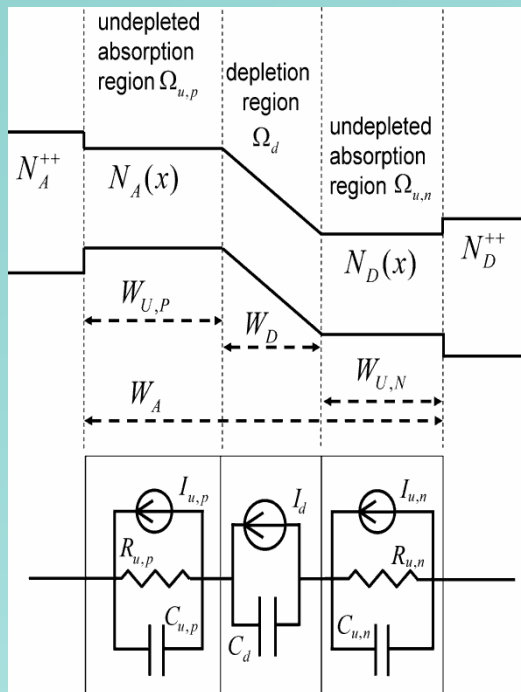
*p-i-n limit  
(fully bipolar)*

*UTC limit  
(fully unipolar)*

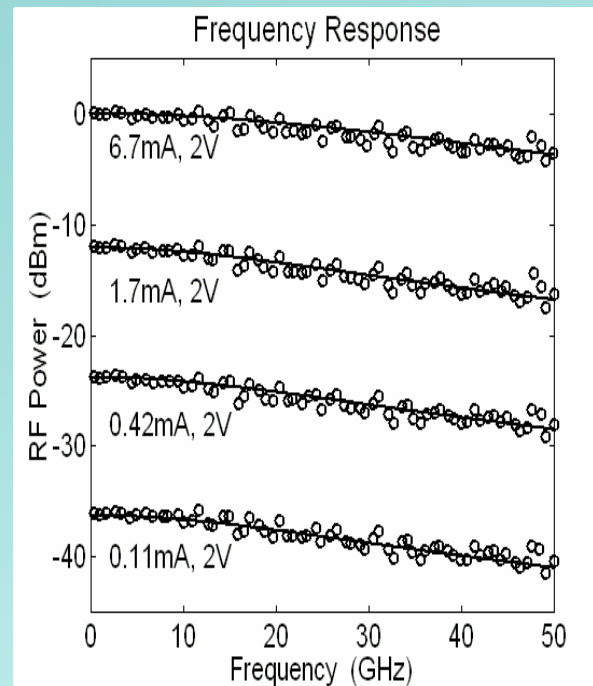


*For fixed  $QE$  and  $C_j$ , optimal 3dB bandwidth is achieved by QU rather than purely unipolar or purely bipolar operation*

# Aside: Application to PDA Designs

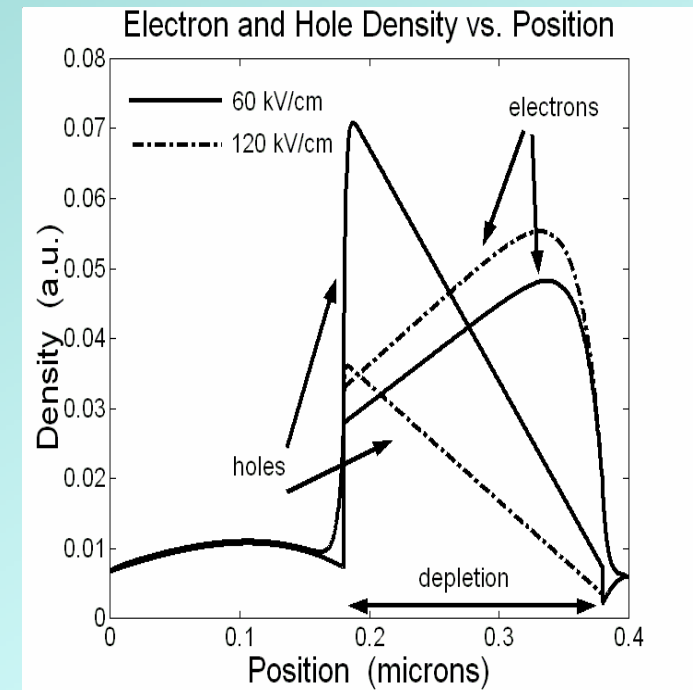


Band diagram and equivalent circuit model



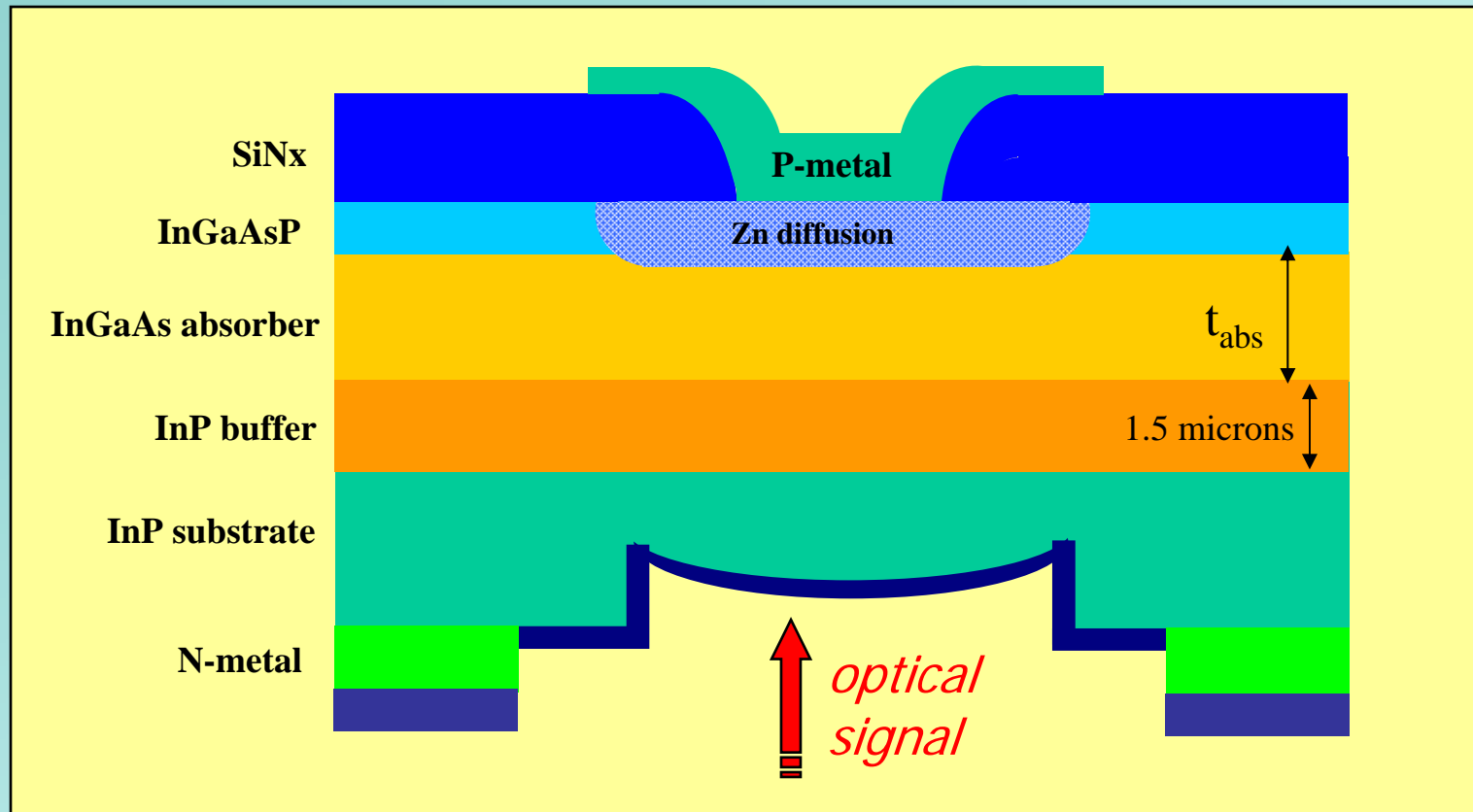
Comparison with experiment

Measurement : X. Li et al., IEEE Photonics Technology Letters, 2004.



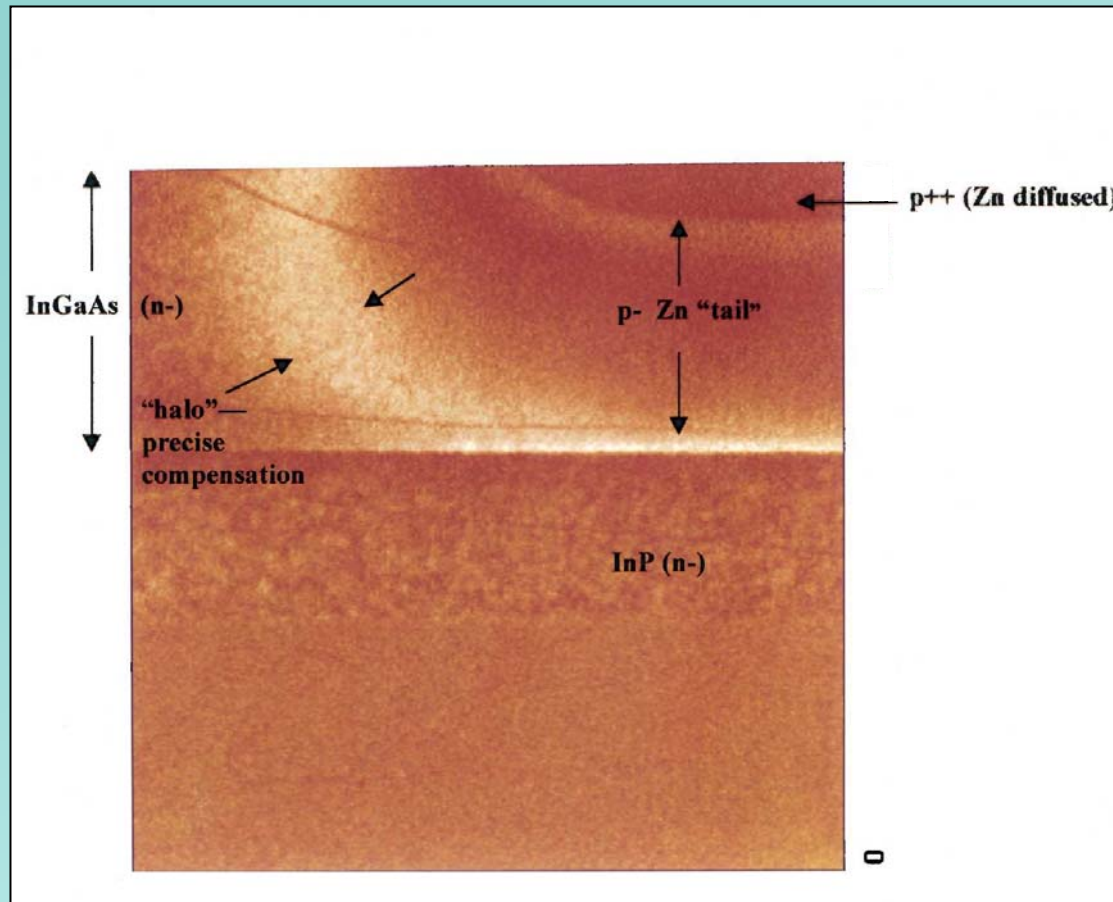
Investigation of "charge balancing"

# Vertical Illumination QU Photodetector



- ★ MOCVD growth
- ★ Post-growth Zn diffusion + thermal anneal

# Scanning Capacitance Measurement

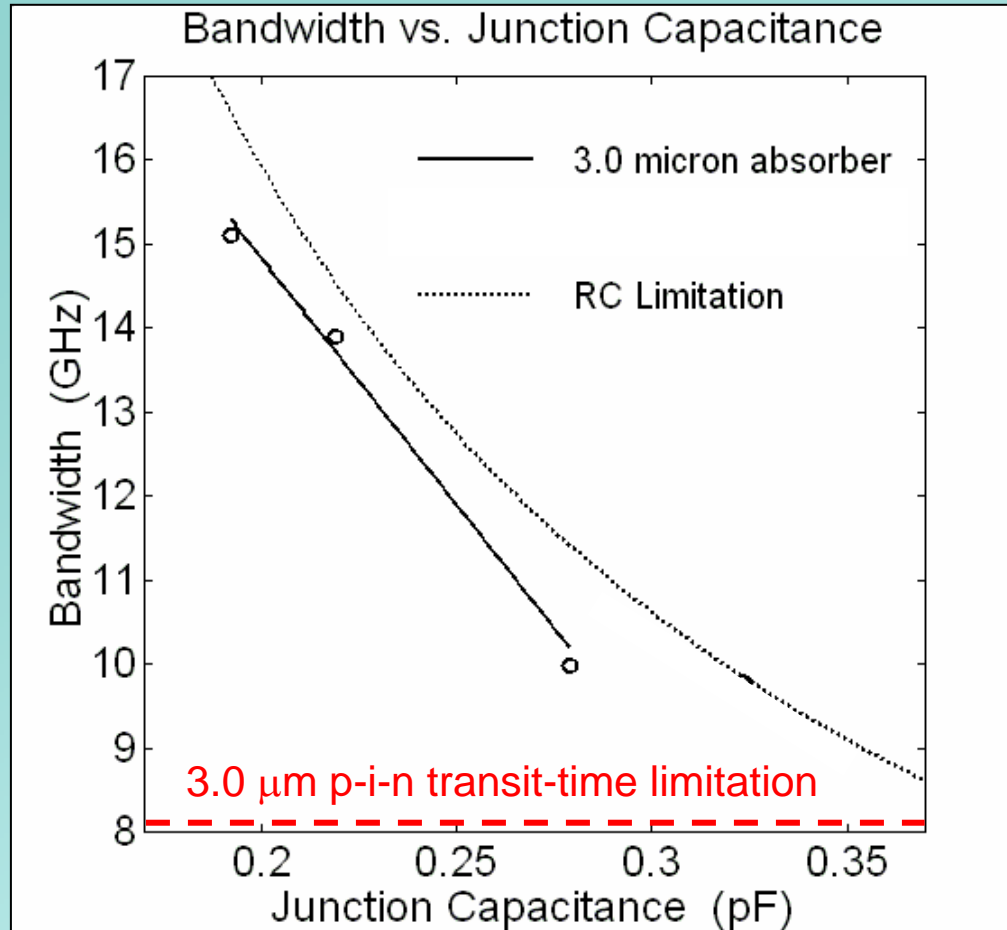


Courtesy of D. V. Lang

- Intensity proportional to free carrier density
- Peripheral "halo" indicates p-n junction at InGaAs/InP interface
- Depletion region straddles InP buffer and InGaAs absorber



# *S12 Measurement at 0 dBm Optical Power*



- *3dB bandwidth far exceeds p-i-n limitations*

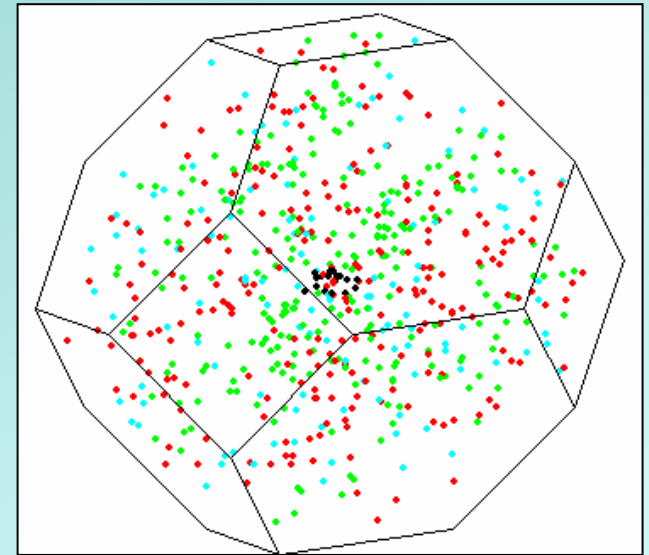
- *QU device is RC-limited*



- *Further BW improvement is possible*

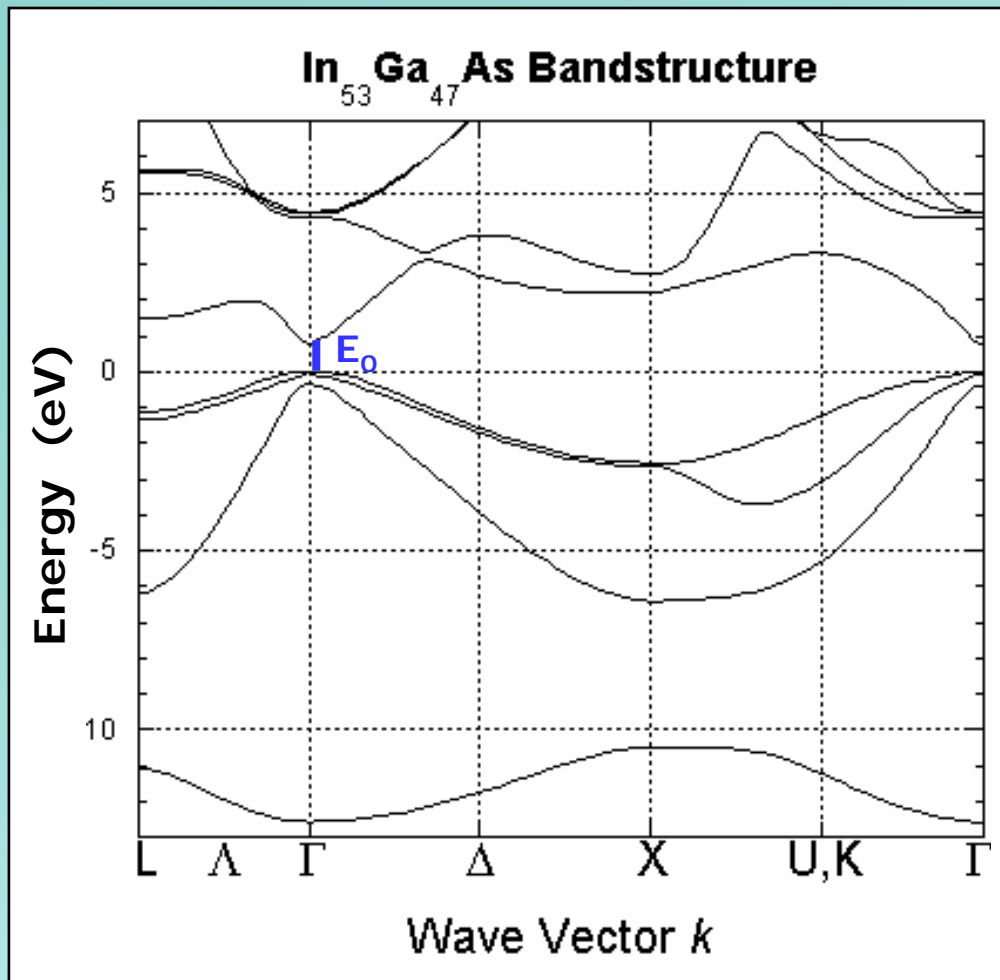
# *Monte Carlo Charge Transport Model*

- *Full band structure of InGaAs and InP*
- *Electron and hole ensemble*
- *Scattering mechanisms:*
  - *Polar optical electron-phonon scattering*
  - *Optical deformation potential scattering*
  - *Inelastic acoustic deformation potential scattering*
  - *Ionized impurity scattering*
- *Exact integration of the linearized BTE to precision of the phase space grids*
- *Mixed-mode simulation, fully coupled to external circuit*



# ***Bandstructure Calculations***

## ***(Nonlocal Empirical Pseudopotential Method w/S-O)***

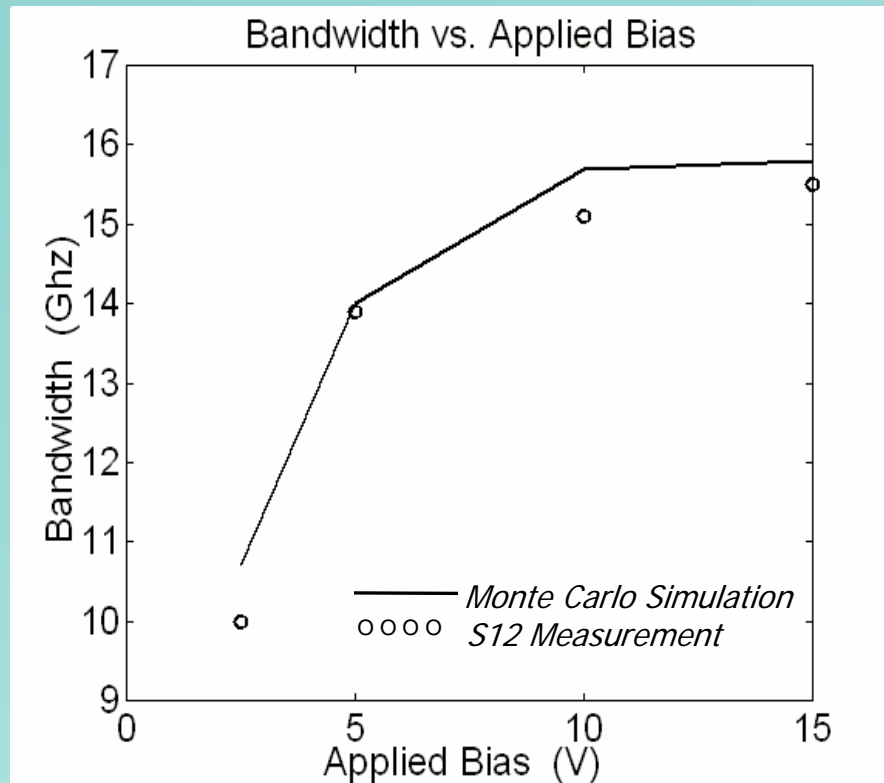


*Developed an algorithm to generate pseudopotential parameters optimized to reproduce measured values of:*

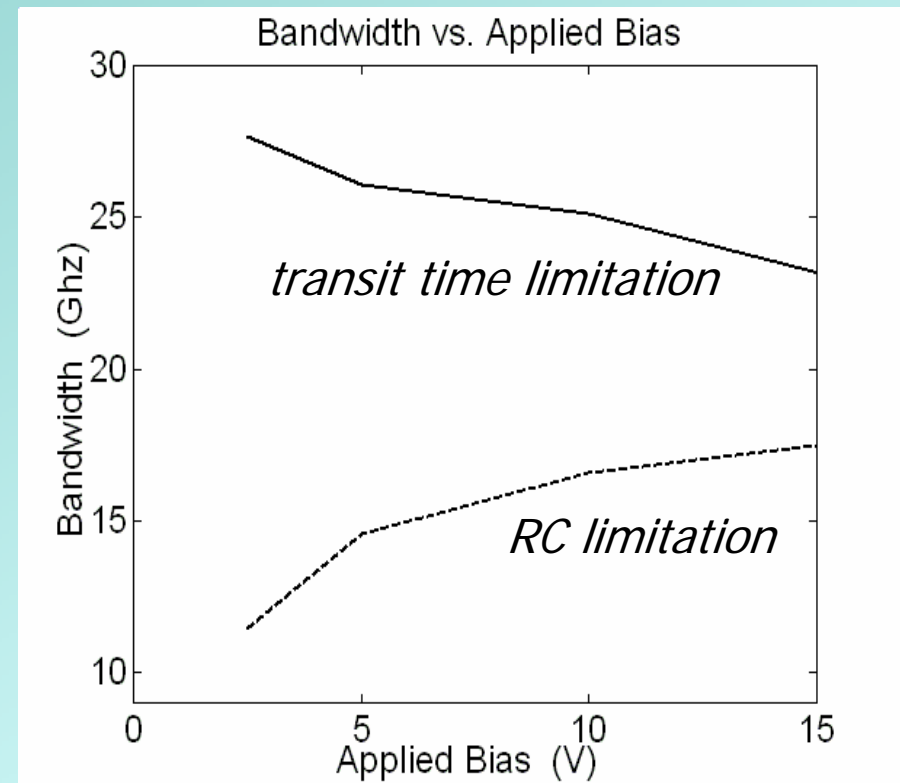
- 1) *Optical transition energies  $E_0$ ,  $E_0 + \Delta_0$ ,  $E_1$ ,  $E_1 + \Delta_1$ ,  $E_0'$ , and  $E_0' + \Delta_0'$  determined by spectroscopic ellipsometry, reflectometry*
- 2) *Effective masses of band-edge electrons and holes, determined by cyclotron resonance*

*New bandstructures generated for  $In_{53}Ga_{47}As$  and  $InP$*

# ***BW vs. Bias with 3.0 $\mu\text{m}$ Absorber***



*Simulation confirms understanding of device operation*



*BW may be improved by increasing  $W_D$  and decreasing  $W_U$*

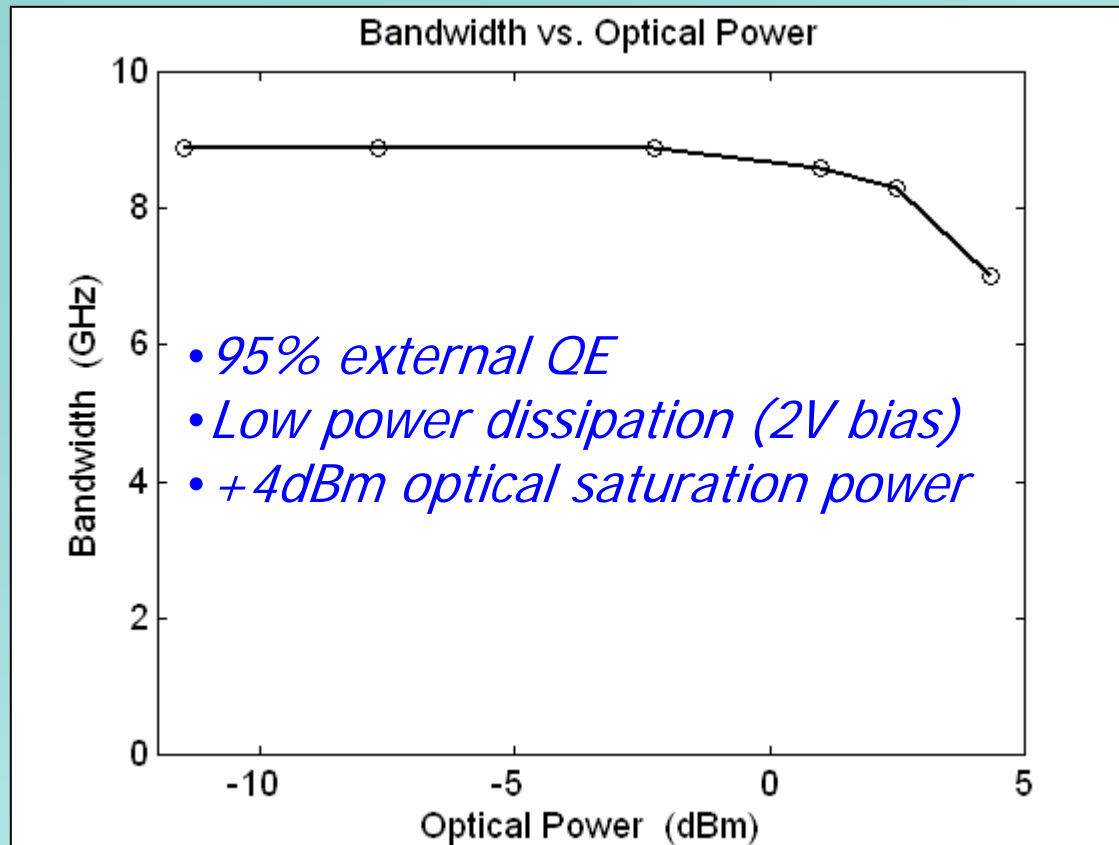
# Summary

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- *QU design strategy proposed as alternative to UTC and p-i-n approaches*
  - *UTC and p-i-n detectors are limiting cases of the QU design strategy*
  - *BW may be maximized by “balancing” electron and hole photocurrent responses.*
- *New equivalent circuit and analytic model proposed for QU and UTC photodiode operation*
- *Device measurements reveal significant improvements in 3dB bandwidth w.r.t. p-i-n design.*

# *Optical Saturation Power*

## *(2.5 $\mu$ m absorber, 2V bias)*

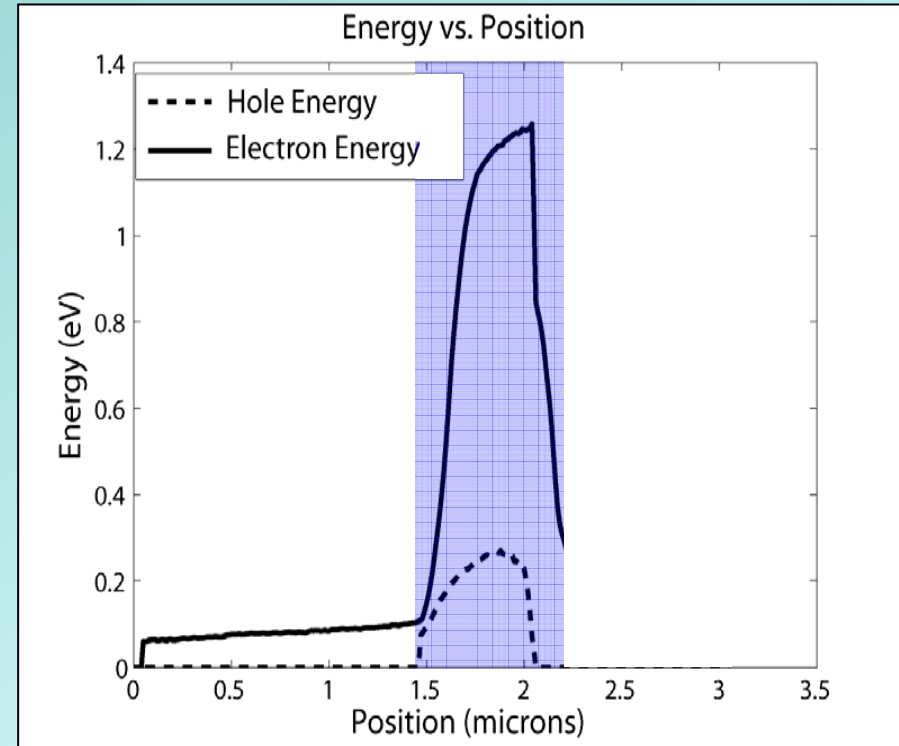
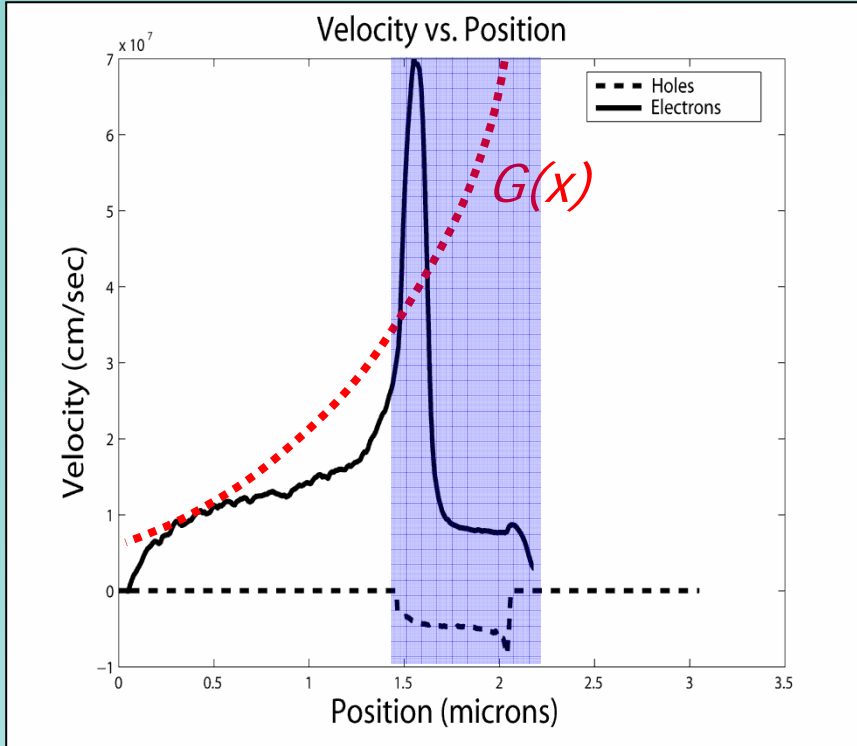


*Bandwidth may be traded for optical saturation power via reduction of  $W_D$  without penalty to quantum efficiency.*

*Highest reported 10 Gbps optical saturation power with 95% QE*

# Monte Carlo Simulation Results

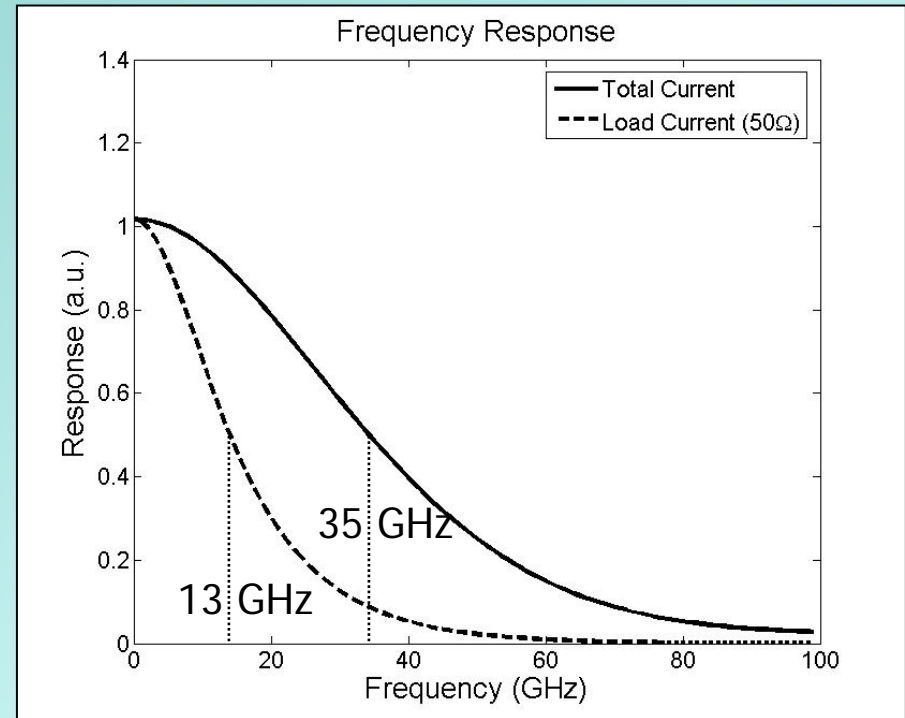
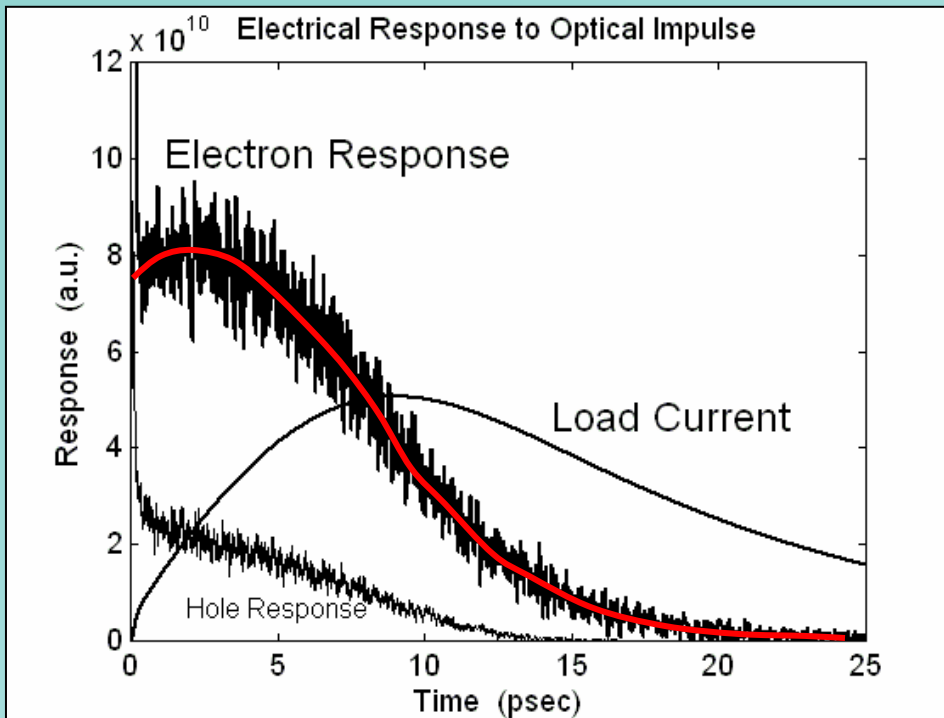
## (2 $\mu\text{m}$ absorber, 5V bias)



*Dopant gradient-induced fields lead to high electron velocity in  $\Omega_U$ .*

*Electron transport is non-local throughout active region*

# *Simulated Impulse/Frequency Response (2 $\mu\text{m}$ absorber, 5V bias)*



*“Balancing” electron and hole response through design of  $W_U$  and  $W_D$  optimizes modulation bandwidth for arbitrary  $W_A$ .*