



Dynamic Internal Optical Field Patterns for Self-Pulsating Two-Section DFB Lasers

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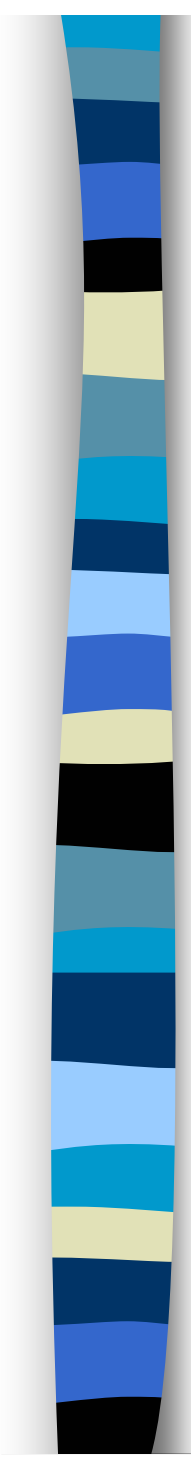


output waveform
vs.
internal optical field pattern

Introduction

- Investigate the mode beating self-pulsation in a two-section distributed feedback (TS-DFB) laser.
- Study the relationship between output waveform and optical field patterns for with/without AR-coating cases.
- It is more **difficult to measure the internal variation inside the device**, especial for the internal optical field analysis in space distribution and in time domain.
- **What is the relationship between output waveform and internal optical field pattern?**

Existed Simulation Tools

- 
- OptiSystem
 - Optical communication system
 - Providing laser module
 - No self-pulsating simulation
 - OptiSim
 - VPItransmissionMaker WDM
VPIcomponentMaker Active Photonics
 - Optical communication system
 - Providing laser module with detailed parameters
 - Transmission Line Laser Model
 - **Providing self-pulsating simulation output waveform**



Optical Field Analysis and Numerical Calculation

1. **Finite-Difference method** works well for laser, with spectral mixing, or with noise.
2. The typical field patterns for the DFB with **$\lambda/4$ phase shift have a peak** on the location of phase shift.
3. The finite difference method could be also applied to **analyze the multi-section DFB**. In addition, setting different section length will create mode depression.

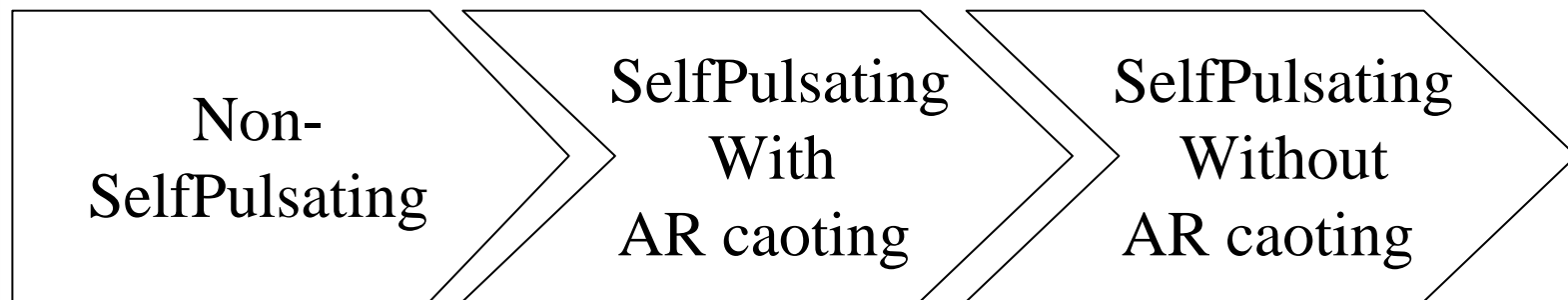


Optical Field Analysis and Numerical Calculation

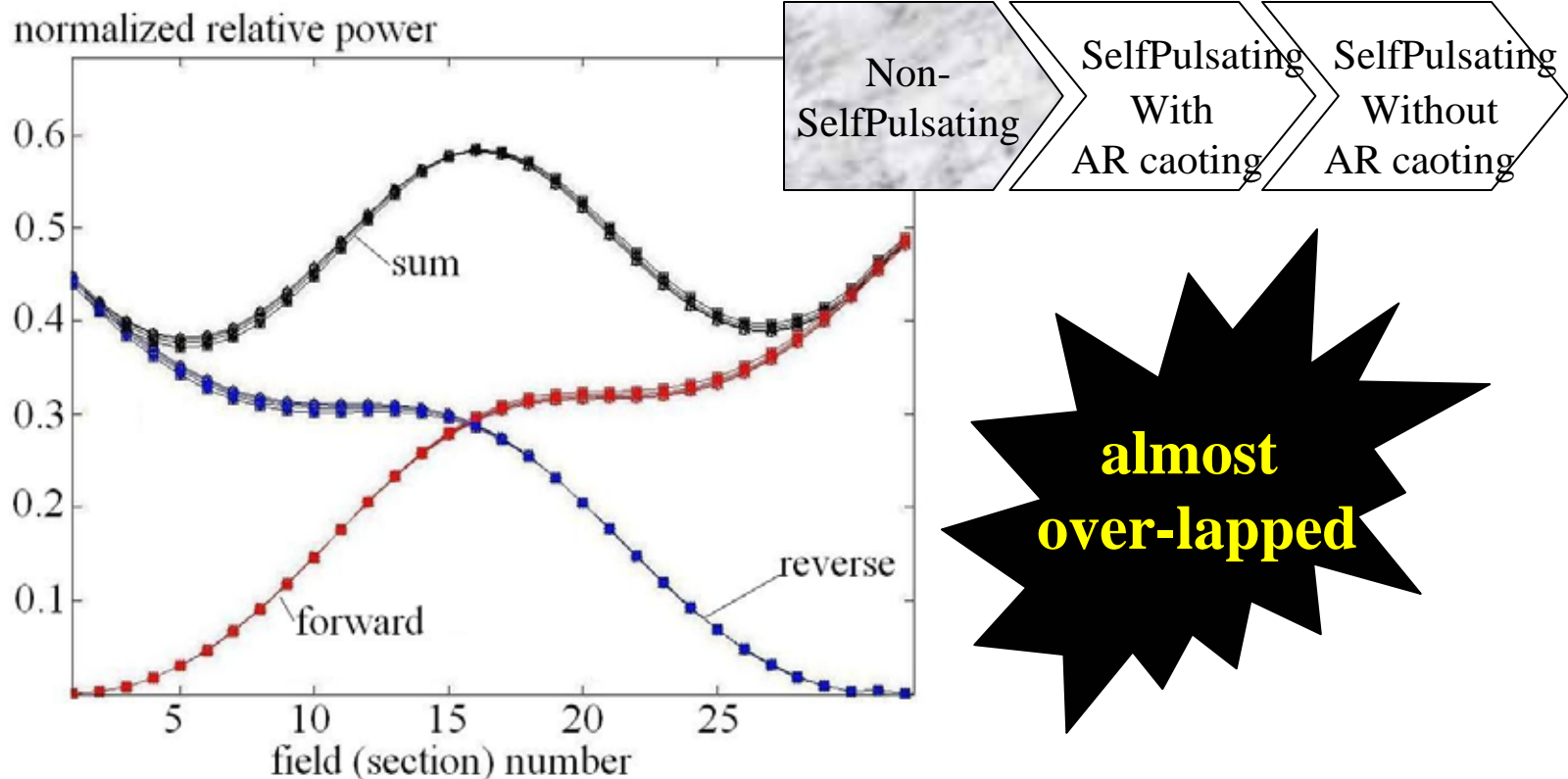
4. In a clock source, the excitation is due to random ‘spontaneous noise’. Hence, the outputs are **not precisely the same for run-to-run, or iterations.**
5. The result traces of iteration-to-iteration could be calculated, and **the accumulative field pattern of all iterations could be visualized.**
6. It is interesting to view the difference between optical field under **non-self-pulsation and optical field under self-pulsation.**

Optical Field Analysis and Numerical Calculation

7. For the former, the **output is stable**. Hence, it is intuitional to image that the optical field should be more stable. That is, for different calculation iterations, the optical field patterns in space should be “**almost overlapped (Case1)**”.
8. For the latter, we consider **two branches: anti-reflective (AR) coating and natural facets**.



Optical Field Analysis and Numerical Calculation **Case1**



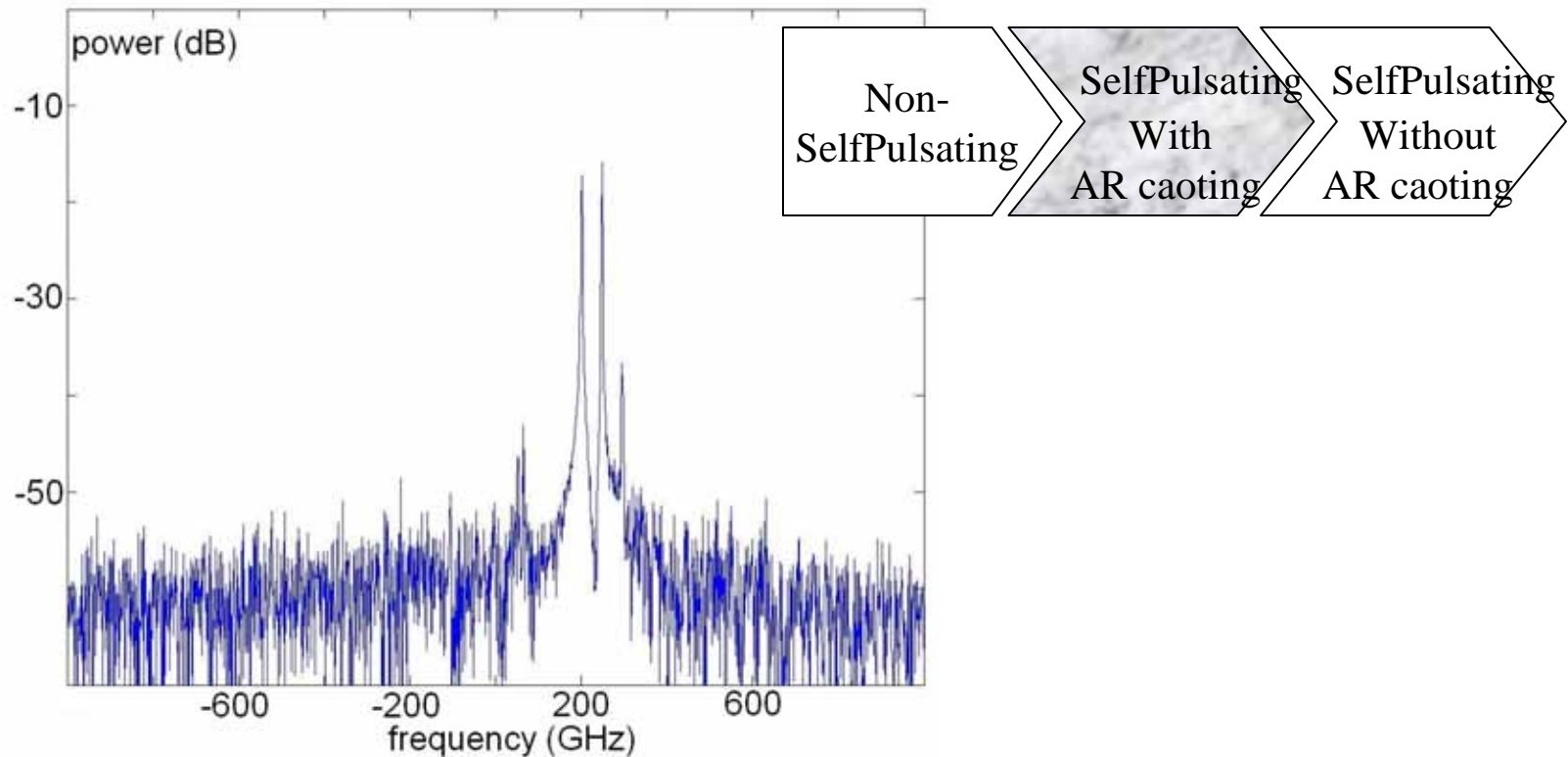
- Calculated normalized space optical field (normalized relative power) for the proposed TS-DFB without self-pulsation, including forward field (from left to right, the leftest point has smallest field), reverse field (from left to right, the leftest point has largest field), and **sum field**.



Optical Field Analysis and Numerical Calculation

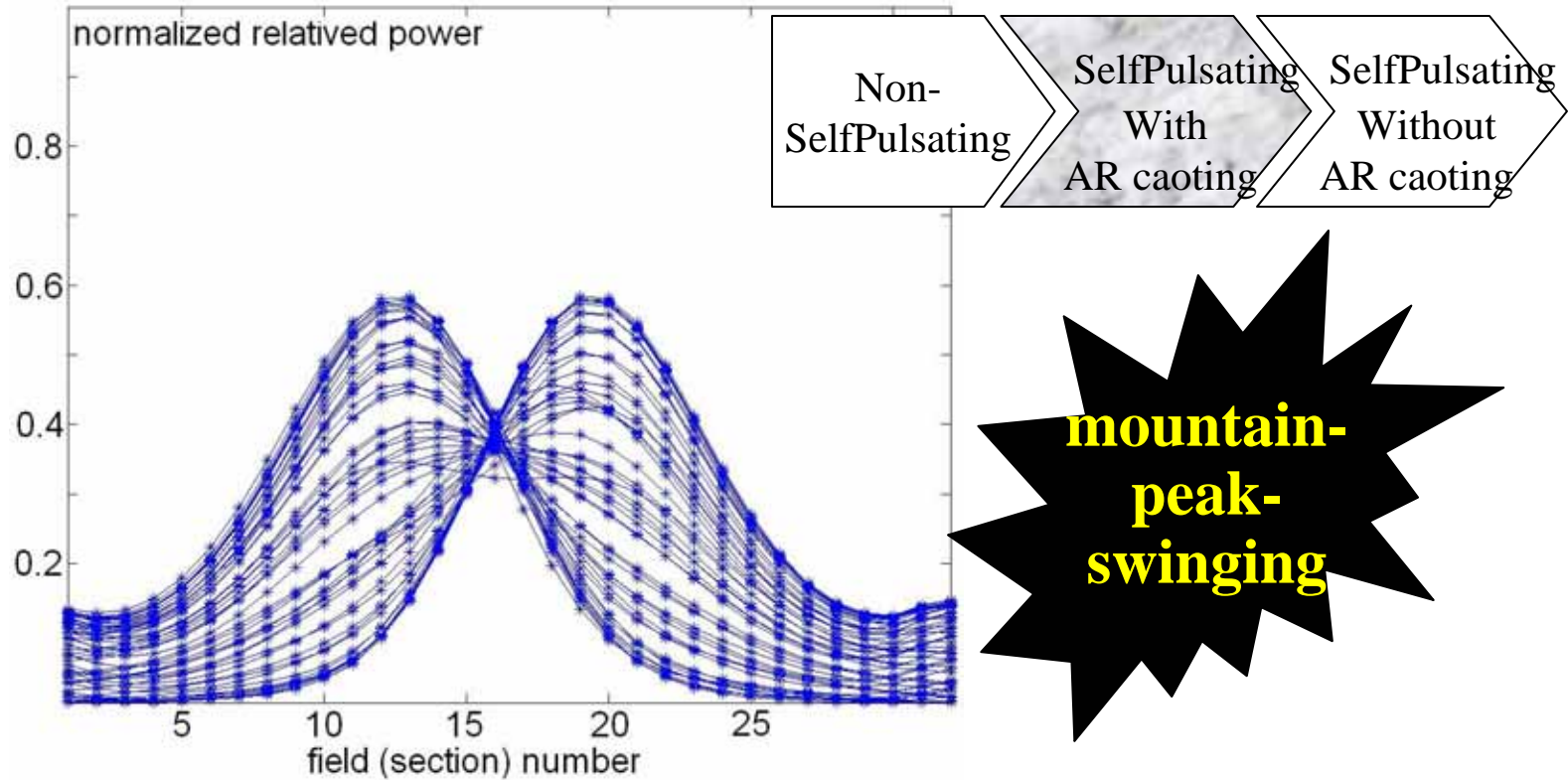
9. The internal optical field patterns should be dynamic for each periodic waveform; that is, it is difficult for the optical field patterns in space to be almost over-lapped. **Instead, it is changed (Case2).**
10. A TS-DFB may be processed with AR coating on both facets. Otherwise, the reflective effect from **natural facets should be considered (Case3).**

Optical Field Analysis and Numerical Calculation **Case2**



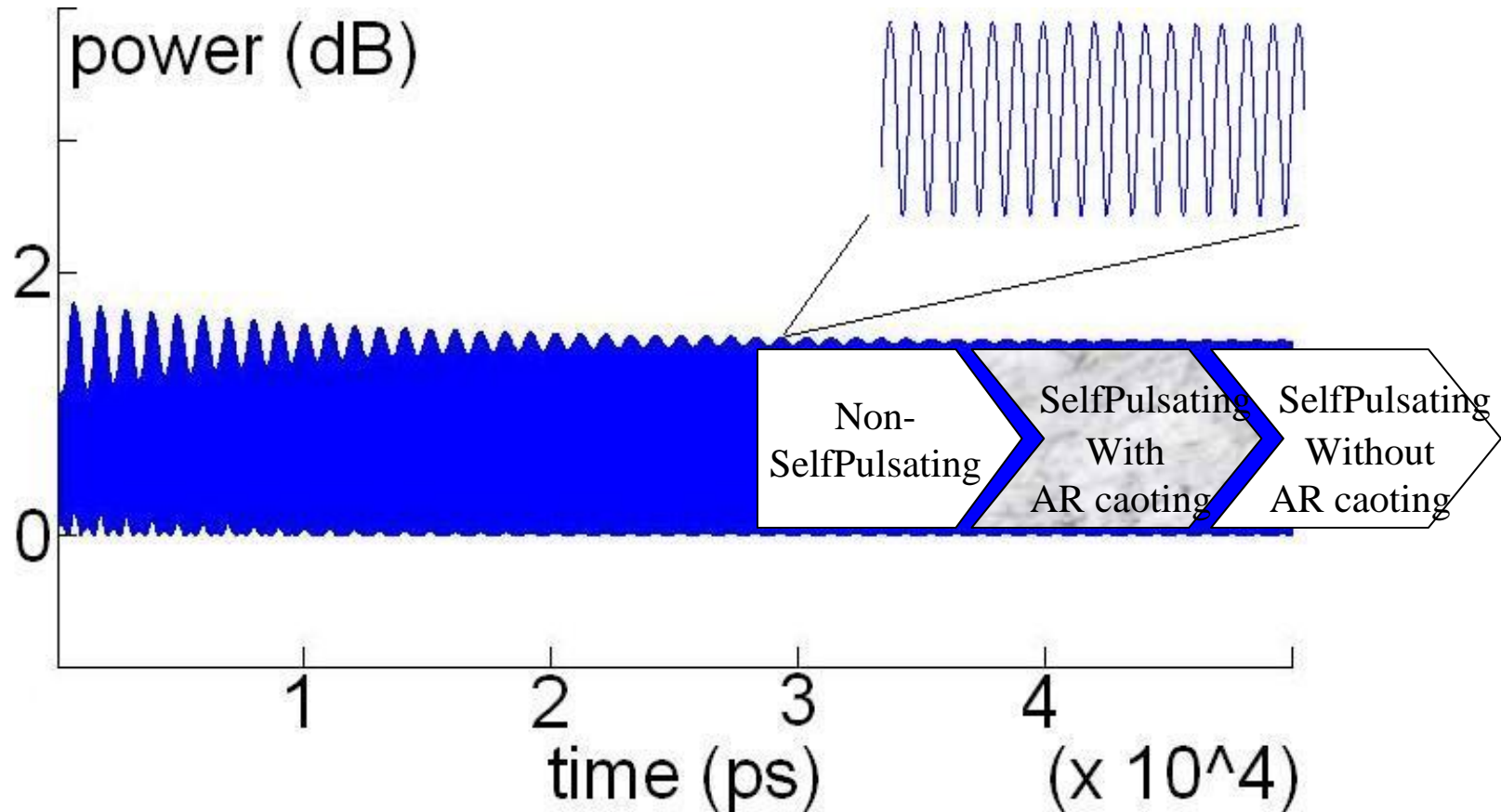
- Calculated normalized optical power spectrum for TS-DFB (with AR-coating) **mode-beating mechanism** under self-pulsation **for long time simulation**. The central wavelength is 1550nm.

Optical Field Analysis and Numerical Calculation **Case2**



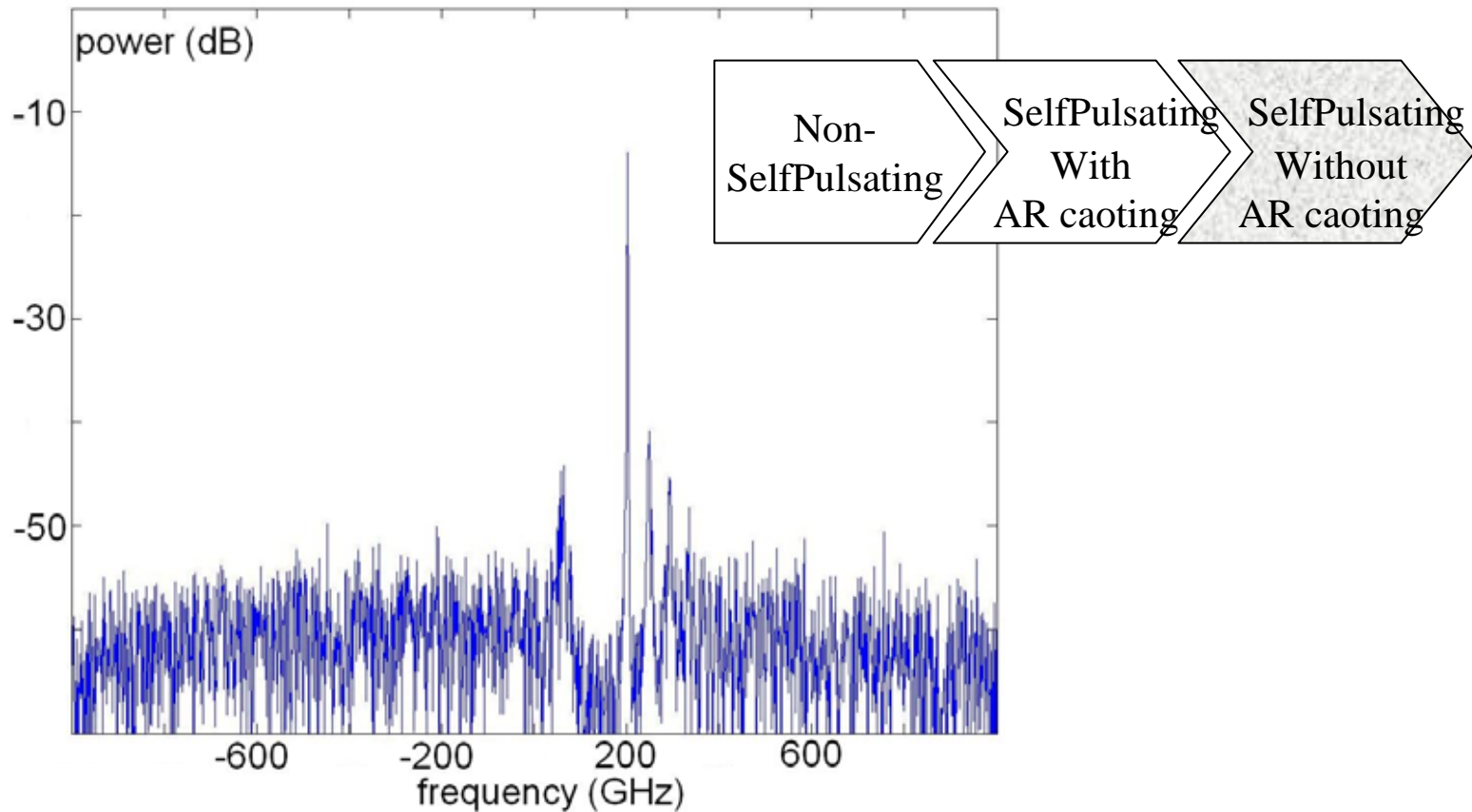
- Calculated normalized space optical sum field (normalized relative power) for TS-DFB including AR-coating, with mode-beating mechanism, and under self-pulsation **for long time simulation**. Two optical fields for **“mountain-peak-swinging”** could be observed.

Optical Field Analysis and Numerical Calculation **Case2**



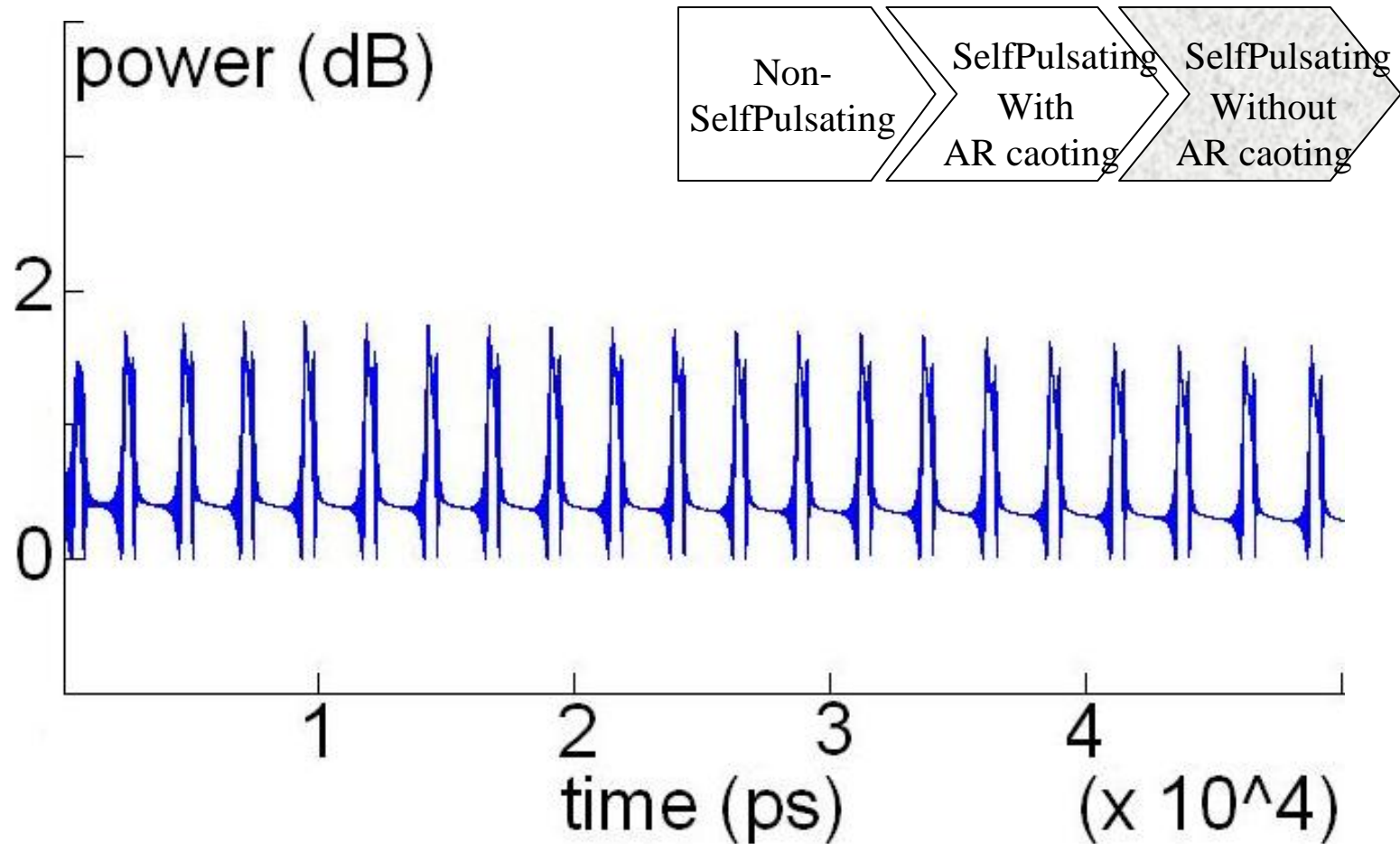
- Calculated normalized periodic optical output waveforms and its detail for TS-DFB mode-beating mechanism, under self-pulsation **for long time simulation**. The pulsation period is **25ps (40GHz)**.

Optical Field Analysis and Numerical Calculation **Case3**



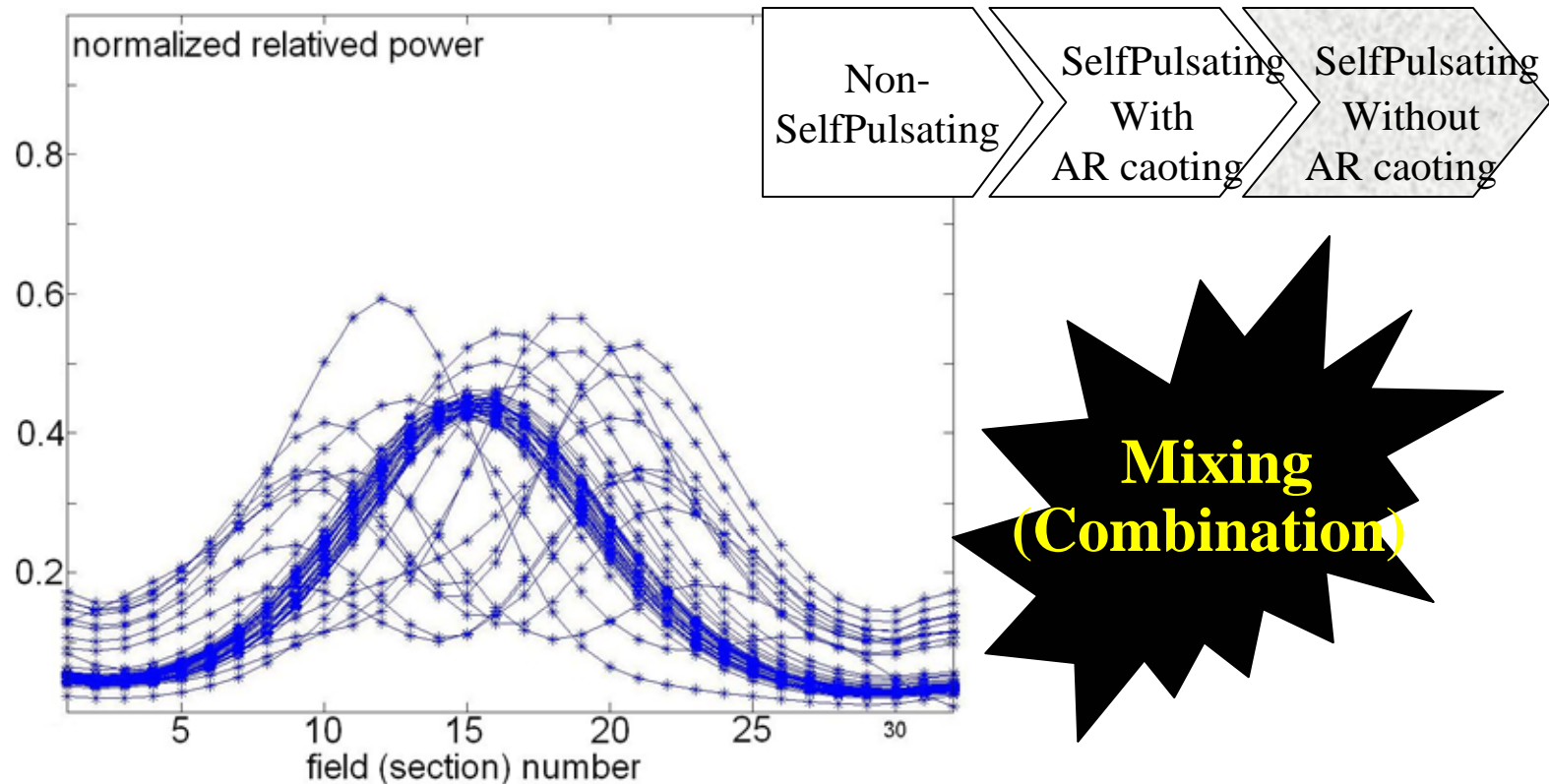
- Calculated normalized optical power spectrum for TS-DFB (with natural facets) under self-pulsation **for long time simulation.**

Optical Field Analysis and Numerical Calculation **Case3**



- Calculated normalized periodic optical output waveforms for TS-DFB (no AR-coating) , under self-pulsation **for long time simulation**.

Optical Field Analysis and Numerical Calculation **Case3**



- Calculated normalized space optical sum field (normalized relative power) for the TS-DFB **including natural facets**, under self-pulsation **for long time simulation**. **Mixing “almost over-lapped” and “mountain-peak-swinging” could be observed.**

Conclusion

- We first apply the Finite-Difference method to DFB internal optical field patterns to study the stable output case.
- Then we analyze the internal optical field patterns of TSDFB under self-pulsation; and our results show that the field patterns also vibrate between two peaks from run-to-run.
- Finally, the difference effect between AR-coating and the natural facets also has been studied.
- In short, **the relationship between output waveform and internal optical field pattern** has been studied.

Reference

- *Sartorius.B, et.al.*, "Dispersive self-Q-switching in self-pulsating DFB lasers," *IEEE Journal of Quantum Electronics*, Vol.33, No.2, pp.211-218, Feb 1998.
- *Marcenac.D.D, et.al.*, "Distinction between multimoded and singlemoded self-pulsations in DFB lasers," *IEEE Electronics Letters*, Vol.30, No.14, pp.1137-1138, July 1994.
- *John Carroll, et. al.*, 'Distributed Feedback semiconductor lasers', chap.7 (1998).

Appendix: Model Math Equations

$$\frac{1}{v_g} \frac{\partial F}{\partial t} + \frac{\partial F}{\partial z} = j\kappa R + (g - j\delta)F + i_{spf}$$

$$\frac{1}{v_g} \frac{\partial R}{\partial t} - \frac{\partial R}{\partial z} = j\kappa F + (g - j\delta)R + i_{spr}$$

$$\begin{bmatrix} F\{(T+1), (Z+1)\} \\ R\{(T+1), Z\} \end{bmatrix} = \exp\{(g - j\delta)s\} \begin{bmatrix} \cos \theta & j \sin \theta \\ j \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} F\{(T, Z)\} \\ R\{T, (Z+1)\} \end{bmatrix}$$

$$\approx \left(\frac{2 + gs - j\delta s}{2 - gs + j\delta s} \right) \begin{bmatrix} \sqrt{1 - \kappa^2 s^2} & j\kappa s \\ j\kappa s & \sqrt{1 - \kappa^2 s^2} \end{bmatrix} \begin{bmatrix} F\{(T, Z)\} \\ R\{T, (Z+1)\} \end{bmatrix}$$

$$\sin \theta = \frac{\kappa s}{1 + \frac{1}{4} \kappa^2 s^2} \approx \kappa s \quad \cos \theta \approx \sqrt{1 - \kappa^2 s^2}$$